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# Reduction behavior of iron oxides in hydrogen and carbon monoxide atmospheres

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### Abstract

The reduction of various iron oxides in hydrogen and carbon monoxide atmospheres has been investigated by temperature programmed reduction ( $TPR_{H2}$  and  $TPR_{CO}$ ), thermo-gravimetric and differential temperature analysis (TG-DTA-MS), and conventional and "in situ" XRD methods. Five different compounds of iron oxides were characterized: hematite  $\alpha$ -Fe $_2O_3$ , goethite  $\alpha$ -FeOOH, ferrihydrite Fe<sub>5</sub>HO<sub>8</sub>-4H<sub>2</sub>O, magnetite  $Fe<sub>3</sub>O<sub>4</sub>$  and wüstite FeO. In the case of iron oxide-hydroxides, goethite and ferrihydrite, the reduction process takes place after accompanying dehydration below 300 °C. Instead of the commonly accepted two-stage reduction of hematite,  $3 \alpha$ -Fe<sub>2</sub>O<sub>3</sub>  $\rightarrow$  2 Fe<sub>3</sub>O<sub>4</sub>  $\rightarrow$  6 Fe, three-stage mechanism  $3Fe_2O_3 \rightarrow 2Fe_3O_4 \rightarrow 6FeO \rightarrow 6Fe$  is postulated especially when temperature of reduction overlaps 570 °C. Up to this temperature the postulated mechanism may also involve disproportionation reaction,  $3Fe^{2+} = 2Fe^{3+} + Fe$ , occurring at both the atomic scale on two-dimensional interface border Fe<sub>3</sub>O<sub>4</sub>/Fe or stoichiometrically equivalent and thermally induced, above 250 °C, phase transformation—wüstite disproportionation to magnetite and metallic iron,  $4FeO \rightleftharpoons Fe_3O_4 + Fe$ . Above 570 °C, the appearance of wüstite phase, as an intermediate of hematite reduction in hydrogen, was experimentally confirmed by "in situ" XRD method. In the case of FeO-H<sub>2</sub> system, instead of one-step simple reduction FeO  $\rightarrow$  Fe, a much more complex two-step pathway FeO  $\rightarrow$  Fe<sub>3</sub>O<sub>4</sub>  $\rightarrow$  Fe up to 570 °C or even the entire sequence of three-step process  $FeO \rightarrow Fe_3O_4 \rightarrow FeO \rightarrow Fe$  up to 880 °C should be reconsidered as a result of the accompanying FeO disproportionation wustite  $\rightleftharpoons$  magnetite + iron manifesting its role above 150 °C and occurring independently on the kind of atmosphere—inert argon or reductive hydrogen or carbon monoxide. The disproportionation reaction of FeO does not consume hydrogen and occurs above 200 °C much easier than FeO reduction in hydrogen above  $350\text{ °C}$ . The main reason seems to result from different mechanistic pathways of disproportionation and reduction reactions. The disproportionation reaction wustite  $\rightleftharpoons$  magnetite + iron makes simple wüstite reduction FeO  $\rightarrow$  Fe a much more complicated process. In the case of thermodynamically forced FeO disproportionation, the oxygen sub-lattice, a closely packed cubic network, does not change during wüstite  $\rightarrow$  magnetite transformation, but the formation of metallic iron phase requires temperature activated diffusion of iron atoms into the region of inter-phase FeO/Fe<sub>3</sub>O<sub>4</sub>. Depending on TPR<sub>H2</sub> conditions (heating rate, velocity and hydrogen concentration), the complete reduction of hematite into metallic iron phase can be accomplished at a relatively low temperature, below 380 °C. Although the reduction behavior is analogical for all examined iron oxides, it is strongly influenced by their size, crystallinity and the conditions of reduction.  $\odot$  2007 Elsevier B.V. All rights reserved.

Keywords: Iron oxide; Reduction process

## 1. Introduction

Many oxidic iron compounds—iron oxides, oxide-hydroxides and hydroxides—not only play an important role in a variety of disciplines and also serve as a model system of reduction and catalytic reactions [\[1\].](#page-9-0) Hematite  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> being a major and thermodynamically most stable oxide among the 16

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identified iron oxidic compounds it is commonly used as an adsorbent, a catalyst precursor and an active component of catalytic material [\[1–6\].](#page-9-0) The CO reduction process of hematitic ores in blast furnace produces metallic iron via a series of intermediate oxides i.e. hematite  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>  $\rightarrow$  magnetite Fe<sub>3</sub>O<sub>4</sub>  $\rightarrow$  wüstite FeO  $\rightarrow$  iron Fe<sup>0</sup>. The reduction of unsupported iron oxides and supported and/or promoted iron catalysts in hydrogen and/or carbon monoxide atmosphere has been studied extensively and plays an important role in many catalytic reactions: ammonia and Fisher-Tropsch synthesis, carbon monoxide hydrogenation, dehydrogenation of ethylbenzene to

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<span id="page-1-0"></span>styrene,  $NO<sub>x</sub>$  and soot removal from diesel exhaust, water gas shift reaction and carbon monoxide oxidation [\[1–5\].](#page-9-0) A considerable attention has been devoted to certain wellestablished features of the transformation of hematite to magnetite, but despite extensive research efforts, the entire mechanism of the hematite reduction in hydrogen is still not fully understood [\[5–41\].](#page-9-0) The nature of the total process is extremely complex and may vary with the physicochemical characteristics of the iron oxide or with the conditions of its reduction [\[5\]](#page-9-0). The literature data diverge considerably since different iron oxides and oxy-hydroxides exist  $(\alpha - Fe_2O_3, Fe_3O_4, FeO, \alpha$ -FeOOH $xH_2O$ , Fe<sub>5</sub>HO<sub>8</sub> $4H_2O$ ), and there are large differences in their reduction process, for instance, temperature range, water partial pressure, particle size and presence of additives or impurities. Iron oxides:  $Fe<sub>2</sub>O<sub>3</sub>$ ,  $Fe<sub>3</sub>O<sub>4</sub>$ ,  $FeO$  not only differ in their fundamental oxidation state but are also usually regarded as nonstoichrometric compounds reflecting their natural tendency for oxidation  $\text{Fe}^{2+} \rightarrow \text{Fe}^{3+}$  (or hydration) and thee appropriate formulas are given in Table 1. The pathway of hematite reduction can be essentially different. The three-step mechanism  $3Fe<sub>2</sub>O<sub>3</sub> \rightarrow 2Fe<sub>3</sub>O<sub>4</sub> \rightarrow 6FeO \rightarrow 6Fe$  is often postulated [\[4–13\]](#page-9-0) instead of the commonly accepted two-step reduction  $3Fe<sub>2</sub>O<sub>3</sub> \rightarrow 2Fe<sub>3</sub>O<sub>4</sub> \rightarrow 6Fe$  [\[13–16\]](#page-9-0). The entirely different pathway of hematite reduction  $3Fe<sub>2</sub>O<sub>3</sub> \rightarrow 6FeO \rightarrow 6Fe$  was also proposed [\[17\]](#page-9-0). In addition, wüstite was accepted as a final product of  $Fe<sub>2</sub>O<sub>3</sub>$  reduction in hydrogen at a temperature range 300–400 °C [\[18\].](#page-9-0) Metastable FeO can be stabilized on the support surface or into iron phase with doping agents [\[19,20\]](#page-9-0). Taking into account the experimental differences, the quantitative and qualitative comparison of TPR profiles for hematite often leads to the unacceptably different conclusions. For example, the approval of two-step reduction  $FeO<sub>1.5</sub> \rightarrow FeO<sub>1.33</sub> \rightarrow Fe$  cannot be favored by TPR<sub>H2</sub> profiles in which unacceptable amounts of hydrogen are consumed in both reduction steps [\[21\].](#page-9-0) Although there are few mechanistic models of hematite reduction in hydrogen and carbon monoxide, common, the lack of certain details referring to the full experimental conformation still remains obvious. Also, there are only sparse and limited literature data referring to the reduction of different kinds of iron oxides, oxide-hydroxides and hydroxides.

This work focusses upon the temperature programmed reduction behavior of five different iron oxidic compounds: hematite  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>, goethite  $\alpha$ -FeOOH, ferrihydrite  $Fe<sub>5</sub>HO<sub>8</sub>·4H<sub>2</sub>O$ , magnetite  $Fe<sub>3</sub>O<sub>4</sub>$  and wüstite FeO in hydrogen and carbon monoxide atmosphere. Although, the above compounds differ in the kind and nature of crystal phase, the presence of hydroxyl groups inside crystal network or on its surface and different oxidation state of iron atoms, one can anticipate rather general mechanistic properties related to the entire reduction process or its fractional reduction stages.

## 2. Experimental

#### 2.1. Materials

Iron(III) oxide  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> (hematite) and iron(III) oxyhydroxides  $\alpha$ -FeOOH· $xH_2O$  (goethite) and Fe<sub>5</sub>HO<sub>8</sub>·4H<sub>2</sub>O (2line ferrihydrite) were prepared from  $Fe(NO<sub>3</sub>)<sub>3</sub>·9H<sub>2</sub>O$  and  $NH<sub>3</sub>$ aqueous solutions by precipitation method and drying at 60 $\degree$ C [\[22\]](#page-9-0). In order to obtain hematite, the calcination of iron oxidehydroxide precursor was done for 3 h at  $600\,^{\circ}\text{C}$  in air. Iron oxide(II) FeO (wüstite) and iron oxide(II, III)  $Fe<sub>3</sub>O<sub>4</sub>$ (magnetite) used as reference materials were purchased from Aldrich company.

#### 2.2. Methods

The surface area measurements were carried out using BET (liquid  $N_2$ ) method. The reduction studies were carried out using: TPR (AMI-1), TG-DTA-MS (Setsys 16/18) and conventional and ''in situ'' XRD methods.

Temperature programmed reduction (TPR $_{H2}$  and TPR<sub>CO</sub>) measurements were carried out in AMI-1 Altamira instrument. Prior to the TPR measurements, catalyst samples (usually 10 or 50 mg) were dried at 60  $\degree$ C and/or calcined for 2 h at 200, 400 and 600 °C, respectively, in air or 10% O<sub>2</sub>–90% Ar gas stream. The iron oxide samples were reduced in 5%  $H_2$ –95% Ar or 5% CO–95% Ar gas mixture with a volume flow rate of  $50 \text{ cm}^3 \text{ min}^{-1}$  and a linear heating rate in the range from O.5 to 25  $\degree$ C/min. TPR<sub>H2</sub> profiles were recorded using thermoconductive detector whereas  $TPR_{CO}$  profiles were recorded with mass spectrometer as a detector. The selected conditions of experiments were chosen to distinguish between mass transfer diffusion and kinetic effects of reduction [\[12,23,24\].](#page-9-0)

Thermo-gravimetric (TG) method equipped with a differential thermal analysis (DTA) device SETSYS-16/18 (Setaram) and a mass spectrometer (MS, Balzers) was used for temperature programmed reduction of iron oxides in different reductive atmospheres: pure hydrogen (99.99%  $H_2$ ) and 5%  $H_2$ –95% Ar or 5% CO–95% Ar gaseous mixtures. The TG– DTA–MS measurements were carried out applying a sample of weight about 10 mg with a linear growth of temperature, usually 1 or 10 $\degree$ C per min, and temperature range from 25 to 1000 °C.

The conventional XRD measurements were carried out on Siemens D5000 powder X-ray diffractometer. It was operating with a scanning speed of  $0.03^{\circ}$  per 10 s. Diffractions patterns

Table 1 Non-stoichiometrical ferric oxides

Mineral	Stoichiometrical formula	Non-stoichiometrical formula
Hematite	$\alpha$ -Fe <sub>2</sub> O <sub>3</sub>	$Fe_{2-x/3}(OH)_{x}O_{3-x}$
Magnetite	Fe <sub>3</sub> O <sub>4</sub>	$\text{Fe}^{\text{II}}_{1-x} \text{Fe}^{\text{III}}_{2+x} \text{O}_{4+x/2}$ $(0 < x \ge 1)$
Wüstite	FeO	Fe <sub>1-x</sub> O (0.83 < 1 - x < 0.95) p = 0.1 MPa, $T > 567$ °C

<span id="page-2-0"></span>were recorded in the range  $2\theta = 10-90^{\circ}$ , using nickel-filtered  $Cu$  K $\alpha$  radiation.

In "in situ" XRD method approximately 200 mg of iron oxide, which had been ground in an agate mortar, was packed in the glass ceramic (Macor) sample holder. Although the reagent gas mixture 5%  $H_2$ –95% Ar was used in the experiment to allow the complete reduction of iron oxide to metallic iron, yet it attenuates the reaction rate enough to allow the collection of an X-ray diffraction pattern at regular intervals. The sample was heated at a nominal rate of  $1 \degree C$  per min. At every 20  $\degree C$  X-ray diffraction data were collected using a PANalytical X'Pert Pro diffractometer equipped with an Anton Paar XRK900 reactor chamber. The electrical heater of the reactor chamber is designed to heat the volume of the sample with a minimal temperature gradient. The X-ray source was a long fine focus X-ray diffraction copper tube operating at 40 kV and 30 mA. Divergent optics were used in a Bragg–Brentano (flat-plate sample) geometry, with fixed divergence  $(1/2^{\circ})$  and antiscatter  $(1^{\circ})$  slits. Incident and receiving 0.04 rad Soller slits were used to limit axial divergence, and a curved graphite monochromator on the receiving side was used to eliminate Cu  $K\beta$  radiation. The sample was scanned at  $3^{\circ}$  per min in the range of  $2\theta$  from  $28^\circ$  to 70°. A PANalytical X'Celerator detector based on Real Time Multiple Strip technology capable of simultaneously measuring the intensities in the  $2\theta$  range of  $2.122^{\circ}$  was used. The analogical procedure was applied during the measurements of temperature activated X-ray phase composition changes in wüstite disproportionation reaction taking place in inert atmosphere of argon.

## 2.3. Quantitative phase analysis

Quantitative phase abundances were determined for hematite, magnetite, wüstite and iron using the High Score Plus package. In quantitative phase analysis using Rietveld method, the weight fraction  $W_i$  of each ith crystalline component in the mixture was calculated from the corresponding refined scale parameter  $S_i$ , according to the equation:

$$
W = \frac{S_i M_i V_i}{\sum S_j M_j V_j},
$$

where  $M_i$  and  $V_i$  are the unit cell mass and volume of *i*th crystalline component, respectively [\[25,26\].](#page-9-0)

#### 3. Results

## 3.1. Hydrogen reduction

The influence of the heating rate, in the range from 0.58 to 10.7 °C per min on TPR $_{H2}$  profiles of hematite is presented in Fig. 1A and B for two sample masses about 50 and 15 mg, respectively.

Using the same volume flow rate of 5%  $H_2$ –95% Ar gas mixture  $(50 \text{ cm}^3 \text{ min}^{-1})$ , the temperature range of the entire reduction of hematite to metallic iron,  $Fe(III) \rightarrow Fe(0)$ , and the changes of TPR profile shape strongly depend on the heating rate. In order to accomplish this process in a low temperature range, up to about 450–480  $\degree$ C, a slow heating rate of 0.58  $\degree$ C per min is required, whereas with a relatively fast heating rate of 10.7  $\mathrm{^{\circ}C}$  per min the complete reduction moves to much higher temperatures, up to about  $700-800$  °C. In less favorable conditions even much higher temperature up to 1250  $\degree$ C was necessary to accomplish reduction of hematite [\[27\].](#page-9-0) The typical  $TPR_{H2}$  profile consists of two fairly well separated reduction peaks, the smaller low temperature peak taking up about 13% of total surface area under TPR curve, reflects the first stage of the reduction of hematite to magnetite  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>  $\rightarrow$  Fe<sub>3</sub>O<sub>4</sub> and the second, broad and much larger, high temperature peak represents the reduction of magnetite to metallic iron  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow \alpha$ -Fe. In fact, in this high temperature region two heavily overlapped peaks can be observed, especially when higher heating rates of 5.52 and 10.7  $\degree$ C per min are applied. These two TPR peaks are tentatively assigned to the two-step magnetite reduction sequence, 2  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow 6 FeO \rightarrow 6 Fe$ . The existence of wustite phase as an intermediate of magnetite reduction was experimentally confirmed by the conventional XRD method when  $TPR_{H2}$  run was interrupted, in temperature range above  $570\textdegree C$  and sample was quickly cooled down in reducing stream (see XRD pattern 6 in [Fig. 6](#page-5-0)). The prolonged contact of reduced hematite sample with hydrogen, accompanying  $TPR_{H2}$  run with low heating rate leads to considerable shift of both TPR peak maxima  $T_{\text{max1}}$  and  $T_{\text{max2}}$ toward lower temperatures, about 120 and 200 $\degree$ C representing the reduction steps  $Fe<sub>2</sub>O<sub>3</sub>$  to  $Fe<sub>3</sub>O<sub>4</sub>$  and  $Fe<sub>3</sub>O<sub>4</sub>$  to Fe, respectively (see broken lines in Fig. 1). The value of maximum temperature  $T_{\text{max}}$  is probably conditioned by a low temperature side of TPR peak representing self-catalyzed nucleation as a rate-determining step [\[14\]](#page-9-0). The first symptoms of hematite reduction may be



Fig. 1. Influence of heating rate on TPR<sub>H2</sub> profiles for  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>: (A) 50 mg; (B) 15 mg; curves: (1) 0.58; (2) 1.07; (3) 2.57; (4) 5.52; (5) 10.7 °C/min.

<span id="page-3-0"></span>

Fig. 2. Influence of heating rate on TPR<sub>H2</sub> profiles for: Fe<sub>3</sub>O<sub>4</sub> (A) and FeO (B); curves: (1) 0.58; (2) 1.07; (3) 2.57; (4) 5.52; (5) 10.7 °C/min.

difficult to recognize as a distinct peak for very low heating rate but the assignment of this TPR peak seems to be beyond any doubts,  $Fe<sub>2</sub>O<sub>3</sub> \rightarrow Fe<sub>3</sub>O<sub>4</sub>$  and the acknowledgment of the second TPR peak can be much more sophisticated than merely direct reduction of magnetite to metallic iron,  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$ . One can anticipate the two-step reduction, magnetite  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow$  wüstite  $Fe_{1-x}O \rightarrow$  iron Fe<sup>0</sup>, occurring when temperature of reduction is higher than 570  $\degree$ C, when wüstite is thermodynamically stable. Such two-step magnetite reduction behavior can be anticipated for rapidly heated samples when diffusion limitations of reduction play an essential role as rate determining factors.

 $TPR_{H2}$  profiles of commercial iron oxides, magnetite and wüstite are presented in Fig. 2A and B, respectively.

In the case of magnetite, the similarity to hematite reduction is obvious (compare [Fig. 1\)](#page-2-0) but the small residual reduction peak located at about 300  $\degree$ C is assigned to the hematite type impurity already present in the original sample of magnetite but not recognizable as appropriate XRD pattern (compare curves 3 and  $4$  in [Fig. 6](#page-5-0)). The reduction of wüstite takes place in the same temperature region as magnetite does, above 320  $\degree$ C. The most characteristic feature of wüstite reduction profile is the more symmetrical shape of the reduction peak in comparison to the TPR<sub>H2</sub> peaks characterizing magnetite and hematite reduction processes, but evident nonsymmetrical tailing on both sides of FeO reduction peak can be observed. In fact, the same temperature range of magnetite and wüstite reductions may suggest their related reduction mechanistic pathways instead of a frequently postulated two-step reduction sequence,  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO \rightarrow Fe.$ 

On the basis of  $TPR_{H2}$  profiles, given in [Figs. 1 and 2,](#page-2-0) the calculated temperature-programmed ''Arhenius plots'' are straight lines for: hematite, magnetite and wüstite  $[45]$ , and they are shown in Fig. 3.

The activation energy can be determined independently of the reduction mechanism applying the position of the TPR peak maximum at different heating rates. And the activation energies of reduction calculated with slope – E/R were 70 and 52 kJ/mol, respectively for hematite two-step reduction  $Fe<sub>2</sub>O<sub>3</sub> \rightarrow Fe<sub>3</sub>O<sub>4</sub>$ and  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$ ; 55 kJ/mol for magnetite reduction  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  and 104 kJ/mol for wüstite reduction FeO  $\rightarrow$  Fe and the evaluated values are rather comparable to those found in literature [\[13–15\].](#page-9-0) The very close obtained values for magnetite reduction and for the second step of hematite reduction seems to confirm the same mechanism of reduction in both cases. The nearly twice higher value of the activation energy of wüstite reduction suggests a considerably different and strongly temperature dependent mechanism.

The comparison of hydrogen reduction behavior of five iron oxidic compounds—two oxy-hydroxides, goethite  $\alpha$ -FeOOH $xH_2O$  and ferrihydrite Fe<sub>5</sub>HO<sub>8</sub>.4H<sub>2</sub>O, and three iron oxides, hematite  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>, magnetite Fe<sub>3</sub>O<sub>4</sub> and wüstite FeO— are illustrated in [Fig. 4](#page-4-0) as  $TPR_{H2}$  profiles with a heating rate of  $1.07 \degree$ C per min and nearly the same mass of sample, about 15 mg.

The mutual differences between TPR profiles reflect both the chemical composition of samples and their bulk and surface properties acquired during sample preparation. In the case of the reduction of ferrihydrite, one can notice rather broad monotonic uptake of hydrogen, above  $150^{\circ}$ C. For goethite the accompanying desorption effect located in temperature range  $150-250$  °C is assigned to the decomposition of nitrate ions which were not washed out entirely during the sample precipitation. The evolution of nitrogen oxides was independently confirmed by the MS method. Despite the expected differences in morphology and the degree of hydration, the  $TPR_{H2}$  profiles of iron(III) oxides and oxy-hydroxides are generally similar.

The results of BET specific surface area for the above iron oxidic compounds are presented in [Table 2](#page-4-0).



Fig. 3. Arhenius plot of  $TPR_{H2}$  profiles for: hematite (1, 2); magnetite (3) and wüstite (4). (1)  $E_a = 70 \text{ kJ/mol}$  for  $Fe_2O_3 \rightarrow Fe_3O_4$ ; (2)  $E_a = 52 \text{ kJ/mol}$  for  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$ ; (3)  $E<sub>a</sub> = 55$  kJ/mol for  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$ ; (4)  $E<sub>a</sub> = 104$  kJ/mol for  $FeO \rightarrow Fe$ .

<span id="page-4-0"></span>

Fig. 4. TPR<sub>H2</sub> profiles for: (1) goethite; (2) ferrihydrite; (3) hematite; (4) magnetite; (5) wüstite; heating rate  $1.07 \degree$ C/min.

The samples of oxy-hydroxides dried at  $60^{\circ}$ C show relatively high surface area  $(20-35 \text{ m}^2/\text{g})$  in accordance with the entirely amorphous structure of ferrihydrite and rather low crystallinity of goethite structure. The hematite sample calcined at 600 °C shows comparable surface area to those characteristic of oxy-hydroxides, but commercial samples magnetite and wüstite show only about 6  $m^2/g$  and below 1  $m^2/g$ , respectively. The particle size of about 0.22  $\mu$ m for magnetite and 1.3  $\mu$ m for wüstite can be estimated assuming spherical and nonporous particles. In fact, a highly dispersed system of wüstite with the crystallites of about 130 nm can be anticipated on the basis of XRD measurements. Thus, instead of a uniform system consisting of the individual and rather similar particles, the different-sized agglomerates of crystallites can be expected.

In order to get a deeper insight into both the reduction and the accompanying dehydration, the additional TG-DTA measurements were carried out. The obtained DTG curves representing the effects of thermal treatment of iron oxidic compounds, in pure hydrogen stream with a linear heating rate  $5^{\circ}$ C per min, are presented in Fig. 5.

In the case of oxy-hydroxides,  $\alpha$ -FeOOH $\cdot xH_2O$  and  $Fe<sub>5</sub>HO<sub>8</sub>·4H<sub>2</sub>O$ , their two-step dehydration occur below  $300 \degree$ C. The second step of ferrihydrite dehydration is heavily overlapped with the first reduction step occurring in the temperature range 150–350 °C (compare also curve 2 in Fig. 4). One can see that the first stage of ferrihydrite and goethite reduction is not strongly influenced by the excessive desorption of water, originating from adsorbed and structural water. After the preparation procedure, these samples were dried only at 60  $\degree$ C. The entire reduction of all samples is accomplished to

Table 2 The results of BET specific surface area for iron oxidic compounds

Iron oxide	Air pretreatment $T_{calc.}$ ( $°C$ )	Surface area $(m^2/g)$
Goethite	60	34.5
Ferrihydrite	60	21.9
Hematite	600	23.5
Magnetite	Commercial	5.6
Wüstite	Commercial	1.0



Fig. 5. DTG curves of reduction in pure hydrogen for: (1) goethite; (2) ferrihydrite;  $(3)$  hematite;  $(4)$  magnetite;  $(5)$  wüstite.

about 550  $\degree$ C. One can notice a symmetrical shape of DTG peak of wüstite reduction in comparison with the rather asymmetrical peaks representing the reduction of remaining samples. The second and dominant reduction effects located in the temperature range  $350-550$  °C are analogous for all samples of iron oxides and oxy-hydroxides.

The XRD patterns of fresh powdered samples of the investigated five oxidic iron compounds are presented as curves 1–5, respectively, in [Fig. 6](#page-5-0) and only the sample of ferrihydrite shows fully amorphous structure.

The "*in situ*" XRD powder diffraction patterns obtained in the course of  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> reduction in hydrogen atmosphere of 5% H2–95% Ar gas stream are illustrated in [Fig. 7](#page-5-0), whereas the calculated changes of phase composition in function of reduction temperature are presented in [Fig. 8](#page-5-0).

In temperature range from 150 to about 400  $\degree$ C the first step of hematite to magnetite reduction,  $3Fe<sub>2</sub>O<sub>3</sub> \rightarrow 2Fe<sub>3</sub>O<sub>4</sub>$ , takes place. At 400  $\degree$ C, the maximal content of magnetite, about 97%, reflects almost the entire disappearance of hematite phase and the very beginning of metallic iron formation. In temperature range of 400–560  $\degree$ C the second step, that is reduction of magnetite to metallic iron, occurs,  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow 3 \alpha$ -Fe, and the resulting gradual decrease in magnetite content is observed in favor of the enhancement of metallic iron formation. At 580  $^{\circ}$ C, the additional wüstite phase appears and three phases are observed: Fe<sub>3</sub>O<sub>4</sub> (53%), FeO (7%) and Fe (40%). Thus, the

<span id="page-5-0"></span>

Fig. 6. XRD patterns for: (1)  $\alpha$ -FeOOH; (2) Fe<sub>5</sub>HO<sub>8</sub>·4H<sub>2</sub>O; (3)  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub>; (4) Fe<sub>3</sub>O<sub>4</sub>; (5) FeO; (6)  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> (after TPR<sub>H2</sub> up to 650 °C); (7)  $\alpha$ -Fe<sub>2</sub>O<sub>3</sub> (after 4 h in pure CO at 500 °C); (8) FeO (after 10 h in Ar at 500 °C); (9) FeO (after TPR<sub>CO</sub> up to 600 °C), where: (\*) getite; ( $\clubsuit$ ) hematite; ( $\spadesuit$ ) magnetite; ( $\spadesuit$ ) wüstite;  $(\nabla)$  iron.

appearance of wüstite phase proves the involvement of a third step in the reduction of hematite, and the simultaneous occurrence of those three phases also confirms a two-step magnetite reduction pathway,  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO \rightarrow Fe$ . The next stage at 600 °C results in the disappearance of  $Fe<sub>3</sub>O<sub>4</sub>$  phase and leads back to two-phase system FeO (41%) and Fe (59%). In the applied conditions of the experiment the reduction of wüstite to metallic iron, FeO  $\rightarrow$  Fe is entirely accomplished at 680 °C.

The same temperature range of both magnetite and wüstite reduction processes (see [Fig. 2A](#page-3-0) and B) and their mutual similarities in  $TPR_{H2}$  behavior seem to be rather contradictive signs for the expected gradual sequence of reduction  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO \rightarrow Fe$ . One can anticipate the involvement of disproportionation reaction  $4FeO \rightleftharpoons Fe_3O_4 + Fe$  during wustite or wüstite like intermediate in the course of magnetite (hematite) reduction. The disproportionation of FeO reflects the formation of both metallic iron phase ( $\text{Fe}^{2+} \rightarrow \text{Fe}^{0}$ ) and a stoichiometrical amount of magnetite phase  $(3Fe^{2+} \rightarrow 2Fe^{3+} + Fe^{2+})$ . The "*in* 



Fig. 7. The "*in situ*" XRD patterns for hematite during temperature programmed reduction in  $5\%$ H<sub>2</sub>–95% Ar.



Fig. 8. Phase composition during "in situ" XRD temperature programmed reduction of hematite in 5%  $H_2$ –95% Ar stream: (1) Fe<sub>2</sub>O<sub>3</sub>; (2) Fe<sub>3</sub>O<sub>4</sub>; (3) FeO; (4) Fe.

situ'' XRD powder diffraction patterns obtained in the course of temperature programmed reduction of commercial FeO in hydrogen atmosphere of 5%  $H_2$ -95% Ar gas stream are presented in Fig. 9, whereas the calculated changes of phase composition in function of reduction temperature are given in [Fig. 10](#page-6-0).

In temperature range of  $150-400$  °C, the simultaneous appearance of  $Fe<sub>3</sub>O<sub>4</sub>$  and Fe phases combined with an appropriate diminishment of FeO phase content and at the same time the lack of wüstite reduction effects prove the occurrence of redox disproportionation of wüstite, not involving hydrogen consumption (compare [Figs. 2B, 8 and](#page-3-0) [9\)](#page-3-0). The mutual changes of molar ratios are close to stoichiometric relations for this reaction. Thus, at still higher temperatures, above 400 $^{\circ}$ C, the uptake of hydrogen can be engaged both in the reduction of wüstite disproportionation product, that is magnetite, and/or in the reduction of the



Fig. 9. The "*in situ*" XRD patterns for wut stite during temperature programmed reduction in 5%H<sub>2</sub>–95% Ar atmosphere, where:  $(\nabla)$  Fe; ( $\triangle$ ) FeO; ( $\spadesuit$ ) Fe<sub>3</sub>O<sub>4</sub>.

<span id="page-6-0"></span>

Fig. 10. Phase composition during temperature programmed reduction of wűstite in 5% H<sub>2</sub>–95% Ar atmosphere: (1) FeO; (2) Fe<sub>3</sub>O<sub>4</sub>; (3) Fe.

remaining wüstite phase. The content of magnetite phase reaches maximum value, slightly above  $500\degree C$ , and goes down to final disappearance at about  $600\degree C$ , and this effect is accompanied by local increase in wüstite content. In the temperature range of  $550-700$  °C the reverse reaction of wüstite disproportionation can be anticipated. Up to 850  $\degree$ C the entire reduction of FeO is accomplished. Thus, depending on temperature, instead of one-step simple reduction  $FeO \rightarrow Fe$ , the much more complex two-step pathway  $FeO \rightarrow Fe_3O_4 \rightarrow Fe$ up to  $570\degree$ C or even the three-step complete sequence FeO  $\rightarrow$  Fe<sub>3</sub>O<sub>4</sub>  $\rightarrow$  FeO  $\rightarrow$  Fe in the range from 150 to 850 °C should be reconsidered as a result of the accompanying wüstite disproportionation 4 FeO  $\rightleftharpoons$  Fe<sub>3</sub>O<sub>4</sub> + Fe manifesting the primary role above  $150^{\circ}$ C and the reversal role from 550 to 700  $\degree$ C. In the course of FeO reduction in hydrogen atmosphere the non-stoichiometric wüstite like  $Fe_{1-x}O$  or magnetite like  $\text{Fe}^{\text{II}}_{1-x}\text{Fe}^{\text{III}}_{2+x}\text{O}_{4+x/2}$  iron oxides were detected, for example Fe<sub>0.920</sub>O, Fe<sub>0.880</sub>O and Fe<sub>2.926</sub>O<sub>4</sub>. During the "in situ" XRD wüstite reduction the particle size of the involved phases undergoes considerable changes in function of the temperature of FeO reduction. The calculated size of metallic iron particles increases monotonically from about 3 nm at 200  $\degree$ C to about 37 nm at 880  $^{\circ}$ C. The initial size of wüstite particles was about 130 nm and decreased to about 50 nm at 300  $^{\circ}$ C, and then a continuous enhancement of particle size was observed to be about 200 nm at 800 °C. The estimated particle size of  $Fe<sub>3</sub>O<sub>4</sub>$ phase was 20–50 nm in the temperature range 300–600  $^{\circ}$ C. The characteristic feature is the comparable sizes of FeO and  $Fe<sub>3</sub>O<sub>4</sub>$ particles.

The transformation of wüstite into magnetite and metallic iron in inert atmosphere of argon (10 h at 500  $^{\circ}$ C) was also experimentally confirmed and an appropriate XRD pattern is presented as curve 8 in [Fig. 6](#page-5-0). The influence of treatment temperature on ''in situ'' XRD powder diffraction patterns obtained in the course of the heating treatment of wüstite in neutral atmosphere of argon is illustrated in Fig. 11.

The metallic iron and magnetite phases can be identified in the temperature range  $200-680$  °C. The additional intermediate XRD reflections and the observed shifts of  $2\Theta$  value locations were attributed to the disordered crystal structure deformation forced by both wüstite disproportionation process and natural tendency of wüstite  $Fe_{1-x}O$  and magnetite  $Fe^{II}_{1-x}Fe^{III}_{2+x}O_{4+x/2}$ changes to their non-stoichiometrical state ([Table 1\)](#page-1-0). The



Fig. 11. The "in situ" XRD patterns for wüstite during temperature programmed treatment in Ar atmosphere, where:  $(\nabla)$  Fe,  $(\triangle)$  FeO,  $(\triangle)$  Fe<sub>3</sub>O<sub>4</sub>.

temperature cycle  $50^{\circ}$ C  $\rightarrow$  800  $^{\circ}$ C  $\rightarrow$  50  $^{\circ}$ C in argon atmosphere seems to confirm the fully reversible character of wüstite disproportionation reaction 4 FeO  $\rightleftharpoons$  Fe<sub>3</sub>O<sub>4</sub> + Fe.

### 3.2. Carbon monoxide reduction

The  $TPR_{CO}$  profiles representing iron oxidic compounds goethite, ferrihydrite, hematite, magnetite and wüstite, obtained with heating rate 1.07 °C per min in 5% CO–95% Ar gas stream are illustrated in Fig. 12.

Temperature programmed reduction profiles reflecting CO consumption were the exact mirror images of evolved  $CO<sub>2</sub>$ , up to 500 °C, and the ion concentration curves  $(m/z = 44)$  are presented in Fig. 12. For goethite, ferrihydrite and hematite samples, the reduction effects located in temperature range 150–300  $\degree$ C are assigned to the first reduction step. The easier reducibility is observed for the hydroxylated samples of



Fig. 12. Carbon dioxide evolution profiles during TPR<sub>CO</sub> in 5% CO–95% Ar atmosphere for (1) goethite; (2) ferrihydrite; (3) hematite; (4) magnetite; (5) wüstite.

<span id="page-7-0"></span>ferrihydrite and goethite. Above 300  $\degree$ C, the second reduction step representing a further reduction takes place. Above 500  $\degree$ C, the additional evolution of  $CO<sub>2</sub>$  was also accompanied by  $CO$ desorption and both the peaks were attributed to surface desorption effects for goethite, ferrihydrite and magnetite samples. In the case of wüstite, a considerably smaller CO reducibility was found and it is confirmed by the  $TPR_{CO}$  profile in [Fig. 12](#page-6-0). The reduced FeO sample after reaching  $620^{\circ}$ C was quenched and finally, the XRD pattern was taken after contact of sample with air at ambient temperature (curve 9 in [Fig. 6](#page-5-0)). As expected, the main unreduced wüstite phase was accompanied by metallic iron as the major reduction product. However, the significant presence of magnetite phase was attributed to wüstite disproportionation reaction  $4FeO \rightarrow Fe<sub>3</sub>O<sub>4</sub> + Fe$  taking place also in reductive atmosphere 5% CO–95% Ar during TPR<sub>CO</sub> run, up to 620 °C. The traces of iron carbide phase Fe<sub>x</sub>C were also detected.

In order to get deeper insight into CO reduction of hematite, the analogical TG–DTA–MS measurements were performed in 5%CO–95% Ar gas stream, and they are presented in Fig. 13 as TG, DTG and DTA curves and MS profiles of ion concentration for CO ( $m/z = 28$ ) and CO<sub>2</sub> ( $m/z = 44$ ), respectively.

Three-step CO reduction of hematite takes place in the temperature range 200–600  $\degree$ C and this process is additionally accompanied by the highly exothermic process of the formation of carbon deposit on the surface of reduced sample, attributed to carbon monoxide disproportionation reaction  $2CO \rightarrow C + CO_2$ occurring above 400  $\degree$ C. Carbon deposition seems to be autocatalyzed by metallic iron produced in final step of hematite



reduction and its efficiency is strongly influenced by the concentration of carbon monoxide gas and the heating rate of sample [\[28\]](#page-9-0). The amorphous graphite like deposit and metallic iron phases, were identified by the conventional XRD method as the final products of hematite reduction, 4 h at 500  $\degree$ C in pure CO (see curve 7 in [Fig. 6\)](#page-5-0). Also, depending on the conditions of carbon diffusion into metallic network (temperature, time) iron carbides  $Fe<sub>x</sub>C$  can be formed, especially when reduction temperature is higher than  $600^{\circ}$ C.

### 4. Discussion

At temperatures below 570  $\degree$ C, the absence of wüstite phase as an intermediate of both hematite and magnetite reduction in hydrogen is not an experimental prerequisite condition during an atomic scale reduction  $\text{Fe}^{3+} \rightarrow \text{Fe}^{2+} \rightarrow \text{Fe}^{0}$  taking place on an interface border between formed metallic iron and reduced magnetite phases Fe/Fe<sub>3</sub>O<sub>4</sub> [\[13,14\]](#page-9-0). During reduction each hydrogen molecule reacts with an interface oxygen atom O<sub>s</sub> giving water molecule and anionic vacancy:

$$
O_s + H_2 \rightarrow \Box + H_2O \tag{1}
$$

A source of electron responsible for reduction step  $Fe^{3+} \rightarrow Fe^{2+}$  could be an interface oxygen vacancy located on  $\text{Fe}^{2+}$  according to an equation representing water desorption step as the result of two hydroxyl group condensation [\[13,14\]:](#page-9-0)

$$
2\,\text{Fe}^{3+} - \text{OH} \rightarrow \text{Fe}^{3+} - \text{O} + \text{Fe}^{2+} + \text{H}_2\text{O} \tag{2}
$$

The above reaction plays significant role not only in the initial dehydration–dehydroxylation processes taking place at the beginning of iron oxy-hydroxides (ferrihydrite and goethite) reduction but it would also be crucial in every reduction stage of iron oxides (hematite, magnetite and wüstite). Usually, in the initial stage of iron oxide reduction, the chemisorptive dissociation of hydrogen molecule is involved resulting in the intermediate hydroxyl group formation according to general scheme:  $2 \quad Q^{2-} + H_2 \rightarrow 2 \text{ OH}^- \rightarrow Q^{2-} + H_2\text{O}$ . Thus, the removal of individual water molecule could serve as a unit measure of iron oxide reduction degree. The same role can be assigned to cationic ratios  $\text{Fe}^{2+}/\text{Fe}^{3+}$  and/or  $\text{Fe}^{0}/\text{Fe}^{2+}$ . The twostep hematite reduction can be represented by the two following equations:

$$
3\alpha - Fe_2O_3 + H_2 \rightarrow 2Fe_3O_4 + H_2O
$$
\n(3)

$$
2 (Fe3O4 + 4 H2 \to 3 Fe + 4 H2O)
$$
 (4)

Formally, the last process of magnetite reduction directly to metallic iron (equation (4)) can be described by a sum of two subsequent steps:

$$
2(Fe3O4 + H2 \rightarrow 3FeO + H2O)
$$
 (5)

$$
6(FeO + H_2 \rightarrow Fe + H_2O)
$$
 (6)

Finally, a sequence of equations (3) and (4) is responsible for the two-step hematite reduction, whereas a sequence of equations (3), (5) and (6) represents the three-step hematite Fig. 13. TG–DTA–MS curves for TPR<sub>CO</sub> hematite reduction. The equations (3)–(6), the same mode of one

hydrogen molecule consumption was applied as equivalent of one oxygen atom removal in general equation [\(1\)](#page-7-0). Taking into account the atomic scale of hematite reduction both reactions  $(5)$  and  $(6)$  would occur whether or not wustite phase is formed. From kinetics point of view slow reaction [\(5\)](#page-7-0) and fast reaction [\(6\)](#page-7-0) would be responsible for the presence of  $Fe<sub>3</sub>O<sub>4</sub>$ and the absence of FeO intermediates in low temperature range of hematite reduction. Above 570  $\degree$ C, the reverse takes place—fast reaction [\(5\)](#page-7-0) and slow reaction [\(6\)](#page-7-0) are responsible for the absence of  $Fe<sub>3</sub>O<sub>4</sub>$  and the appearance of  $FeO$ intermediates.

In low temperature range wüstite is unstable phase and above 150 °C it is partially transformed into  $Fe<sub>3</sub>O<sub>4</sub>$  and Fe phases as a result of disproportionation reaction not consuming hydrogen:

$$
4 \text{FeO} \rightleftharpoons \text{Fe}_3\text{O}_4 + \text{Fe} \qquad \Delta G^0 = -6.9 \text{ kJ} \text{ mol}^{-1} \tag{7}
$$

The high temperature treatment of wüstite up to  $780^{\circ}$ C in inert atmosphere confirms the reversible character of temperature activated process of disproportionation. The reduction of wüstite to metallic iron in hydrogen or carbon monoxide is not a simple one-step process because it is accompanied by disproportionation reaction regardless of the fact of reductive atmosphere. At low temperature, above  $150^{\circ}$ C, the disproportionation reaction takes place whereas in most cases reduction of magnetite starts above  $350^{\circ}$ C. In such situation instead of one-step simple reduction  $FeO \rightarrow Fe$ , a much more complex two-step process  $FeO \rightarrow Fe_3O_4 \rightarrow Fe$  up to 570 °C or even a three-step reduction  $FeO \rightarrow Fe_3O_4 \rightarrow FeO \rightarrow Fe$  will operate up to  $850^{\circ}$ C.

The presence of water and its partial pressure in hydrogen stream  $H_2O/H_2$  play a crucial role not only affecting the kinetics of water desorption and its diffusion but also influencing the thermodynamics of the system  $Fe<sub>2</sub>O<sub>3</sub>/Fe<sub>3</sub>O<sub>4</sub>/Fe<sub>x</sub>O/Fe$ . Both the retardation of reduction  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  and the acceleration of H<sub>2</sub> dissociation by metallic Fe and the subsequent hydrogen spillover by  $H_2O$  can influence the reduction kinetics in negative and/or positive way, respectively [\[13,16,29\].](#page-9-0)

Below 570  $\degree$ C, the experimentally evidenced presence of thermodynamically unstable wüstite as an intermediate of the reduction of an unsupported iron(III) oxidic compounds is rather seldom in literature. The low temperature formation of wüstite, below 500 °C was observed during the reduction of magnetite and hematite  $[30,31]$ . The presence of wüstite in the oxidized form of iron catalysts for ammonia synthesis (doped with  $Al_2O_3$ ,  $SiO_2$ , CaO and  $K_2O$ ) is rather common [\[32–34\]](#page-9-0). Frequently, wüstite appears in bi-oxide systems or iron supported catalysts. The stabilization of metastable wüstite phase on oxidic support surface  $(MgO, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>)$  is considered as an indication of strong FeO—support interphase interactions or solid solutions and/or appropriate chemical compounds [\[10,26,28,35–43\].](#page-9-0) Often, the low loaded samples of iron oxide/support catalysts hardly ever revealed the presence of metallic iron phase after high temperature reduction of catalyst in hydrogen or carbon monoxide atmospheres.

According to Spitzer et al. [\[5\]](#page-9-0) when the sample is reduced at a temperature above 700  $\degree$ C in the usual topochemical way oxygen weight loss occurs at three reaction interfaces  $Fe/Fe<sub>x</sub>O$ ,  $Fe<sub>x</sub>O/Fe<sub>3</sub>O<sub>4</sub>$  and  $Fe<sub>3</sub>O<sub>4</sub>/Fe<sub>2</sub>O<sub>3</sub>$ . The mechanism of iron-oxide reduction leads to a rather the unavoidable conclusion that the nature of the total process is extremely complex and may vary with the physico-chemical characteristics of oxide specimen or with the conditions of reduction.

The hydrogen reduction behavior of  $Fe<sub>2</sub>O<sub>3</sub>$ ,  $Fe<sub>3</sub>O<sub>4</sub>$  and  $FeO<sub>4</sub>$ is strongly influenced by the temperature–time–pressure dependent process. According to some literature sources, the only intermediate is magnetite, whereas others postulate both magnetite and wüstite. As FeO is thermodynamically unstable below 576 °C [\[44\]](#page-10-0), any reduction beyond  $Fe<sub>3</sub>O<sub>4</sub>$  should give Fe metal and this is the case in the presented paper [\[19\]](#page-9-0). Only when the Fe<sub>2</sub>O<sub>3</sub> phase disappears the reduction of Fe<sub>3</sub>O<sub>4</sub> to Fe can be observed. The present data show that during the first stage of hematite reduction one-third of  $Fe<sup>3+</sup>$  ions are reduced to  $Fe<sup>2+</sup>$  ions. Our experimental data prove the existence of FeO phase above  $570\,^{\circ}\text{C}$  as an intermediate in the course of  $Fe<sub>3</sub>O<sub>4</sub>$  reduction regardless of diffusion or kinetic limitations. In temperature range  $350-570$  °C instead of direct magnetite reduction to iron,  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$ , the two-step process is still possible, at least in atomic scale on the surface of magnetite. Assuming the reversible character of FeO disproportionation 4 FeO  $\rightleftharpoons$  Fe<sub>3</sub>O<sub>4</sub> + Fe, the coexistence of both reaction products,  $Fe<sub>3</sub>O<sub>4</sub>$  and Fe in direct contact, which is the case of magnetite reduction in hydrogen, should result at least in FeO surface species located in the interface region between  $Fe<sub>3</sub>O<sub>4</sub>$  and Fe. The formation of ordered FeO (1 1 1) domains as intermediate reduction species on  $Fe<sub>3</sub>O<sub>4</sub>$  surface was reported [\[44\].](#page-10-0) The disproportionation reaction: wüstite  $\rightleftharpoons$  magnetite + iron makes simple wüstite reduction  $FeO \rightarrow Fe$  a more complicated process. In the case of thermodynamically forced FeO disproportionation the cubic sub-lattice of oxygen atom network does not change during wüstite  $\rightarrow$  magnetite transformation and only the process of metallic iron phase formation requires temperature activated diffusion of iron atoms into the inter-phase FeO/  $Fe<sub>3</sub>O<sub>4</sub>$  region.

## 5. Conclusions

The approach of the temperature dependent reduction mechanism is common for all iron oxides (Fe<sub>2</sub>O<sub>3</sub>, Fe<sub>3</sub>O<sub>4</sub>, FeO) or iron oxy-hydroxides (FeOOH, Fe<sub>5</sub>HO<sub>8</sub>.4H<sub>2</sub>O) after a lowtemperature dehydration ( $\langle 300 \degree C \rangle$ ). The key factor the temperature  $570 \degree C$  is the lowest border limit of the thermodynamic stability of FeO. Below that temperature FeO disproportionation reaction,  $4FeO \rightarrow Fe<sub>3</sub>O<sub>4</sub> + Fe$  is shifted toward products, whereas above that temperature the reverse reaction  $Fe<sub>3</sub>O<sub>4</sub> + Fe \rightarrow 4FeO$  dominates. The disproportionation reaction occurs in neutral atmosphere and although it does not involve hydrogen but it can influence the mechanism of the reduction of iron oxides in hydrogen. Depending on the reduction temperature the proposed paths of <span id="page-9-0"></span>iron oxides reduction can be assigned to the following schemes:

Hematite:

 $Fe<sub>2</sub>O<sub>3</sub> \rightarrow Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  (below 570 °C)  $Fe<sub>2</sub>O<sub>3</sub> \rightarrow Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO \rightarrow Fe$  (below and above 570 °C) Magnetite:  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe (below 570 °C)$ 

 $Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO \rightarrow Fe$  (below and above 570 °C) Wüstite:

 $FeO \rightarrow Fe_3O_4 \rightarrow Fe$  (below 570 °C) FeO  $\rightarrow$  Fe<sub>3</sub>O<sub>4</sub>  $\rightarrow$  FeO  $\rightarrow$  Fe (below and above 570 °C) FeO  $\rightarrow$  Fe (below and above 570 °C)

The first step of  $Fe<sub>2</sub>O<sub>3</sub> \rightarrow Fe<sub>3</sub>O<sub>4</sub>$  reduction requires the transformation of oxygen sub-lattice combined with iron atoms dislocation. The second step of  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  reduction requires the nucleation sites of metallic Fe phase. The third step of  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow FeO$  reduction does not require any transformation of oxygen sub-lattice. It can take place at higher temperatures than 570  $\degree$ C. Also, the reverse disproportionation of FeO favors this reaction but an essential role is attributed to an interface in direct contact of magnetite with metallic iron, and such border does exist in the second step of  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  reduction and in this way this reduction step can be replaced by the reverse disproportionation of FeO. The mechanism of  $FeO \rightarrow Fe$ reduction is relatively simple but only at temperatures higher than 570  $\degree$ C. A much complicated process of FeO reduction is in simpler case a sequence of two-step  $FeO \rightarrow Fe_3O_4 \rightarrow Fe$  or even, three-step  $FeO \rightarrow Fe_3O_4 \rightarrow FeO \rightarrow Fe$  reduction. The first step in both cases refers to FeO disproportionation starting above  $150^{\circ}$ C and in this way the additional substrate of a subsequent reduction,  $Fe<sub>3</sub>O<sub>4</sub>$  is formed and equivalent Fe atoms, serving as nucleation sites of metallic iron phase are created. Thus, two parallel reduction paths are possible:  $Fe<sub>3</sub>O<sub>4</sub> \rightarrow Fe$  and  $FeO \rightarrow Fe$  in low-temperature range and only one-path  $FeO \rightarrow Fe$  reduction at high-temperatures but only after the accomplishment of the reverse FeO disproportionation,  $Fe<sub>3</sub>O<sub>4</sub> + Fe \rightarrow 4FeO$ . The much higher energy of the activation of FeO reduction (104 kJ/mol) indirectly indicates much more temperature resistant process in comparison with hematite reduction (70 kJ/mol, 52 kJ/mol) and magnetite reduction (55 kJ/mol).

The thermodynamic instability of FeO rather refers to the state of FeO after the formation an appropriate conditions, usually in high temperature, and its final quenching in low temperature conditions. The stable and highly dispersed FeO phase in Fe/support catalyst can be obtained as a result of the strong chemical surface interaction between FeO and support. The additives can play a crucial role in stabilizing FeO particles in magnetite phase. The appearance of FeO crystal phase as an intermediate compound of iron(III) oxide reduction was experimentally confirmed by XRD method above  $570^{\circ}$ C. Depending on hydrogen reduction conditions, the complete reduction of hematite into metallic iron phase can be accomplished even at low temperature up to  $380^{\circ}$ C in pure hydrogen. Although the reduction behavior is analogical for all examined iron oxides it is strongly influenced by their particle size, crystallinity and the conditions of the temperature–time– pressure dependent reduction.

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